

MAE40 - Linear Circuits - Winter 22
Final Exam, March 14, 2022

Instructions

- (i) Prior to the exam, you must have completed the Academic Integrity Pledge at <https://academicintegrity.ucsd.edu/forms/form-pledge.html>
- (ii) The exam is open book. You may use your class notes and textbook
- (iii) Collaboration is not permitted. The answers you provide should be the result only of your own work
- (iv) On the questions for which the answers are given, please provide detailed derivations
- (v) The exam has 4 questions for a total of 40 points and 4 bonus points
- (vi) You have from 11:30am to 2:30pm to complete the exam. Allow sufficient time to post your answers in Canvas (submission closes at 2:40pm).
- (vii) If there is any clarification needed, post your question in the “Discussions” tab of the class Canvas webpage (“Clarifications on question statements of final”)

Good luck!

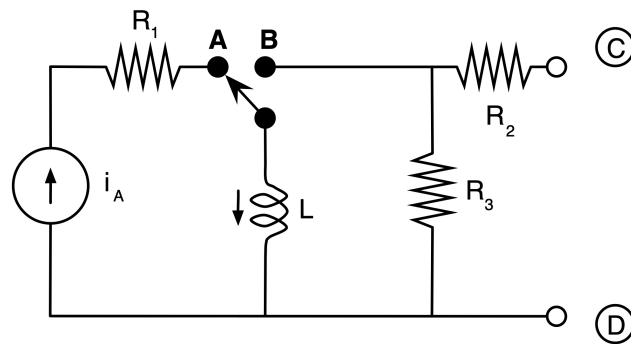


Figure 1: Circuit for Question 1.

1. Equivalent Circuits

Consider the circuit depicted in Figure 1. The value i_a of the current source is constant. The switch is kept in position **A** for a very long time. At $t = 0$, it is moved to position **B**.

Part I: [2 points] Find the initial condition $i_L(0)$ for the inductor.

Part II: [2 points] Transform the circuit in Figure 1 into the s -domain, using a voltage source to account for the initial condition of the inductor.

Part III: [2 points] For the circuit you obtained in Part II, find the open-circuit voltage transform as seen from terminals **C**-**D**. The answer should be given as a ratio of two polynomials.

Part IV: [2 points] For the circuit you obtained in Part II, find the short-circuit current transform as seen from terminals **C**-**D**. The answer should be given as a ratio of two polynomials.

Part V: [2 points] For the circuit you obtained in Part II, find the Thevenin equivalent in the s -domain as seen from terminals **C**-**D** (the impedance should be given as a ratio of two polynomials).

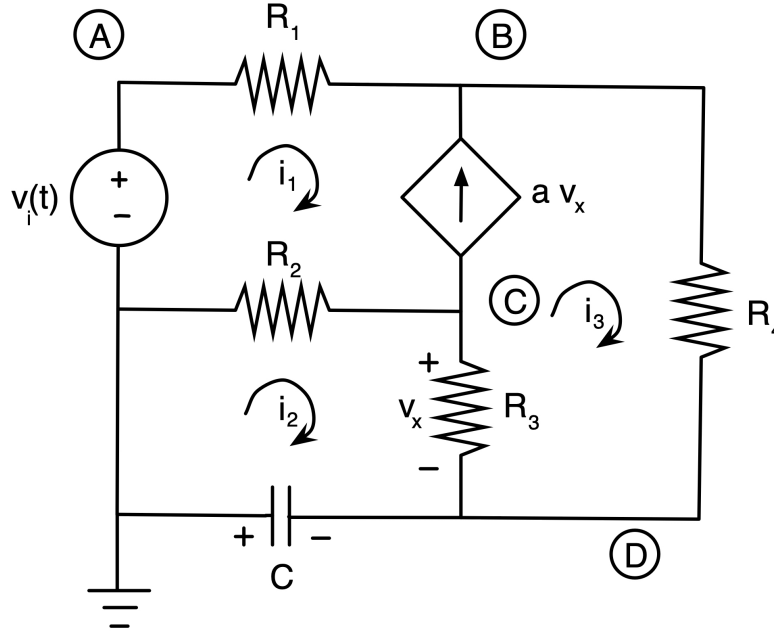


Figure 2: Nodal and Mesh Analysis Circuit for Question 2. a is a known positive constant.

2. Nodal and Mesh Analysis on the s -domain

- Part I:** [5 points] Convert the circuit in Figure 2 to the s -domain and formulate its node-voltage equations. Use the reference node and other labels as shown in the figure. *Do not assume zero initial conditions.* Make sure your final answer has the *same* number of independent equations as unknown variables (notice the presence of the dependent source). No need to solve any equations!
- Part II:** [5 points] Convert the circuit in Figure 2 to the s -domain and formulate its mesh-current equations. Use the mesh currents shown in the figure. *Do not assume zero initial conditions.* Make sure your final answer has the *same* number of independent equations as unknown variables (notice the presence of the dependent source). No need to solve any equations!
- Part III:** [Extra 2 points] Express the capacitor's voltage transform $V_C(s)$ in terms of the node voltages. Do the same in terms of the mesh currents.

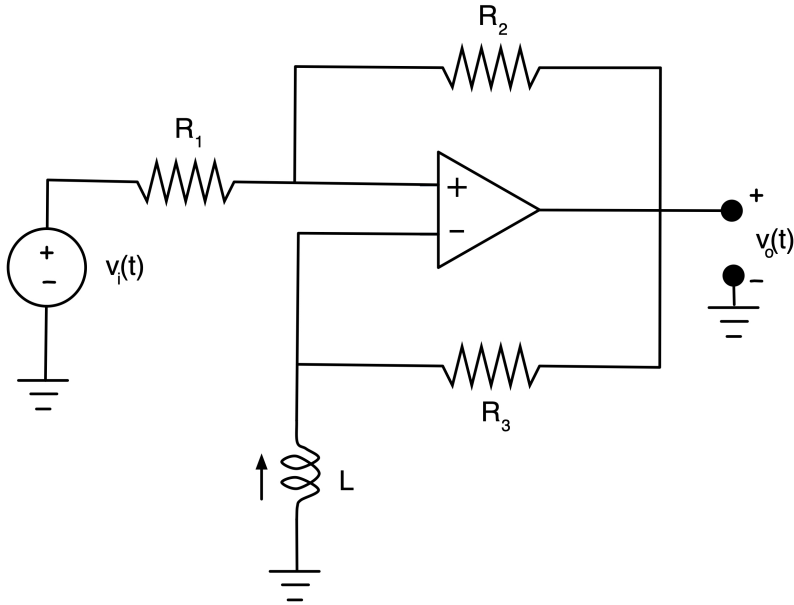


Figure 3: RL circuit for Laplace Analysis for Question 3.

3. Laplace Domain Circuit Analysis

Part I: [2 points] Consider the circuit depicted in Figure 3. The initial condition of the inductor is given by

$$i_L(0^-) = 1A.$$

Use this initial condition to transform the circuit into the s -domain for $t \geq 0$. Use an equivalent model for the inductor in which the initial condition appears as a voltage source.

Part II: [3 points] Use nodal analysis to show that the output response transform $V_o(s)$ as a function of $V_i(s)$ is expressed as

$$V_o(s) = -\frac{R_2(R_3 + sL)}{R_1R_3 - R_2Ls}V_i(s) + \frac{(R_1 + R_2)R_3L}{R_1R_3 - R_2Ls}$$

Part III: [3 points] Use partial fractions and inverse Laplace transforms to show that the output voltage $v_o(t)$ when $v_i(t) = e^{-2t}u(t)$ V, $L = 1$ H, and $R_1 = R_2 = R_3 = 1 \Omega$ is

$$v_o(t) = \frac{1}{3}(e^{-2t} - 4e^t)u(t).$$

Part IV: [2 points] Decompose the output voltage of Part III as (i) the sum of the natural and forced response, and (ii) the sum of the zero-state and zero-input response.

4. OpAmp Design and Chain Rule

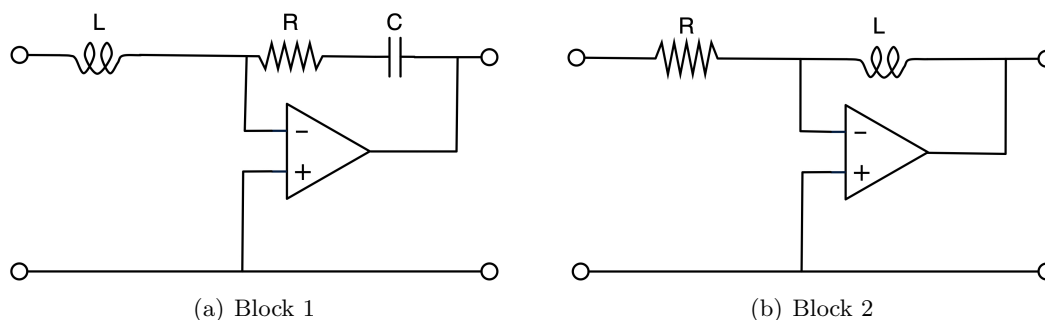


Figure 4: Circuits for Question 4.

Part I: [2 points] Find the transfer functions $T_1(s)$ and $T_2(s)$ for each block in Figure 4.

Part II: [2 points] If you were to connect the blocks in series in the following two configurations: (a) (block 1, block 2) and (b) (block 2, block 1), will you obtain the same transfer function? Why?

Part III: [3 points] An engineer used a configuration from Part II whose transfer function is

$$T(s) = T_1(s) \cdot T_2(s) = \frac{RCs + 1}{RCs}$$

However, the engineer was surprised to observe that when a source circuit with Thévenin equivalent $V_T(s)$ and $Z_T(s)$ was connected, the output transform was different from

$$V_o(s) = T(s)V_T(s)$$

which is what the engineer had expected. Can you explain why?

Part IV: [3 points] Eventually, the engineer gave up on the blocks above and came up with a different design for realizing $T(s)$. The engineer did so by employing resistors with value R and capacitors with values C , and a single op-amp. When the source circuit with Thévenin equivalent $V_T(s)$ and $Z_T(s)$ was hooked up to the design, the engineer finally got the expected output transform $V_o(s) = T(s)V_T(s)$. Can you reproduce the design?

Part V [Extra 2 points] Compute the steady-state response $v_o^{SS}(t)$ of your circuit in Part IV when $R = 1 \Omega$, $C = 1 \text{ F}$, and $v_T(t) = 5 \cos(3t + \frac{\pi}{2})$.